## In the Claims

Claims 1-24 (Cancelled)

- 25. (Currently Amended) A hot-rolled steel plate containing C of about 0.03 to about 0.1%, Si of about 0.01 to about 0.5%, Mn of about 1.2 to about 2.5% and Al of about 0.08% or less by mass, wherein a metal structure is a substantially three-phase structure of ferrite, bainite, and island martensite, and an area fraction of the island martensite is about 3 to about 20%, in addition, the steel plate comprises a complex carbide precipitated in the ferrite phase and further comprises either has any one of chemical composition conditions of the following (1) to (3) for precipitating a complex carbide in a ferrite phase:
  - and Ti of about 0.005 to about 0.04%, wherein the remainder is substantially Fe, and C/(Mo+Ti) which is a ratio of C amount to total amount of Mo and Ti in percent by atom is 1.2 to 3;
  - a condition where the steel plate further contains Mo of about 0.05 to about 0.4% and Ti of about 0.005 to about 0.04%, in addition, contains Nb of about 0.005 to about 0.07% and/or V of about 0.005 to about 0.1%, wherein the remainder is substantially Fe, and C/(Mo+Ti+Nb+V) which is a ratio of the C amount to total amount of Mo, Ti, Nb and V in percent by atom is 1.2 to 3; and,
  - a condition where the steel plate further contains at least two selected from Ti of about 0.005 to about 0.04%, Nb of about 0.005 to about 0.07% and V of about 0.005 to about 0.1%, wherein the remainder is substantially Fe, and C/(Ti+Nb+V) which is a ratio of the C amount to total amount of Ti, Nb and V in percent by atom is 1.2 to 3.
- 26. (Currently Amended) A hot-rolled steel plate containing C of about 0.03 to about 0.1%, Si of about 0.01 to about 0.5%, Mn of about 1.2 to about 2.5%, Al of about 0.08% or less,

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Mo of about 0.05 to about 0.4% and Ti of about 0.005 to about 0.04% by mass, wherein the remainder is substantially Fe, and C/(Mo+Ti) which is a ratio of C amount to total amount of Mo and Ti in percent by atom is 1.2 to 3, and a metal structure is a substantially three-phase structure of ferrite, bainite, and island martensite and an area fraction of the island martensite is about 3 to about 20% and further comprises a complex carbide precipitated in the ferrite phase.

- 27. (Currently Amended) A hot-rolled steel plate containing C of about 0.03 to about 0.1%, Si of about 0.01 to about 0.5%, Mn of about 1.2 to about 2.5% and Al of about 0.08% or less by mass, and containing at least two elements selected from Ti of about 0.005 to about 0.04%, Nb of about 0.005 to about 0.07% and V of about 0.005 to about 0.1% by mass, wherein the remainder is substantially Fe, and C/(Ti+Nb+V) which is a ratio of C amount to total amount of Ti, Nb, and V in percent by atom is 1.2 to 3, and a metal structure is a substantially three-phase structure of ferrite, bainite, and island martensite and an area fraction of the island martensite is about 3 to about 20% and further comprises a complex carbide precipitated in the ferrite phase.
- 28. (Previously Presented) The hot rolled steel plate according to any one of claims 25 to 27, wherein any one of the following complex carbides is precipitated in the ferrite phase:
  - (a) a complex carbide containing Ti and Mo, having a grain diameter of less than about 10nm;
  - (b) a complex carbide containing Ti, Mo, Nb and/or V, having a grain diameter of less than 10nm; and,
  - (c) a complex carbide containing at least two elements selected from Ti, Nb and V, having a grain diameter of less than 10nm.
- 29. (Previously Presented) The hot rolled steel plate according to any one of claims 25 to 27, wherein the steel plate further contains N of about 0.007% or less by mass.

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- 30. (Previously Presented) The hot rolled steel plate according to claim 26, wherein the steel plate further contains Nb of about 0.005 to about 0.07% and/or V of about 0.005 to about 0.1% by mass, and C/(Mo+Ti+Nb+V) that is the ratio of the C amount to the total amount of Mo, Ti, Nb and V in percent by atom is 1.2 to 3.
- 31. (Previously Presented) The hot rolled steel plate according to any one of claims 25 to 27, wherein the steel plate contains Ti of about 0.005 to less than about 0.02%.
- 32. (Previously Presented) The hot rolled steel plate according to any one of claims 25 to 27, wherein the steel plate further contains at least one of Cu of about 0.5% or less, Ni of about 0.5% or less, Cr of about 0.5% or less, B of about 0.005% or less, and Ca of about 0.0005 to about 0.003% by mass.
- 33. (Previously Presented) The hot rolled steel plate according to any one of claims 25 to 27, wherein the steel plate further contains Ti/N of about 2 to about 8 in percent by mass.
- 34. (Previously Presented) A welded steel pipe using the steel plates according to any one of claims 25 to 27.
  - 35. (Withdrawn) A method for manufacturing a hot-rolled steel plate, comprising:

hot-rolling a steel slab, which contains C of about 0.03 to about 0.1%, Si of about 0.01 to about 0.5%, Mn of about 1.2 to about 2.5%, and Al of about 0.08% or less, and further has any one of chemical composition conditions of the following (1) to (3) to precipitate complex carbides in the ferrite phase, at a condition of heating temperature of about 1000 to about 1300°C and rolling finish temperature of about Ar3 or more;

performing accelerated cooling of the hot-rolled steel plate to about 450 to about 650°C at a cooling rate of about 5 °C/sec or more:

and reheating the steel plate to about 550 to about 750°C at a heating rate of about 0.5 °C/sec or more promptly after the cooling:

- a condition where the steel plate further contains Mo of about 0.05 to about 0.4% and Ti of about 0.005 to about 0.04%, wherein the remainder is substantially Fe, and C/(Mo+Ti) which is a ratio of C amount to total amount of Mo and Ti in percent by atom is 1.2 to 3;
- and Ti of about 0.005 to about 0.04%, and contains No of about 0.005 to about 0.07% and/or V of about 0.005 to about 0.1%, wherein the remainder is substantially Fe, and C/(Mo+Ti+Nb+V) which is a ratio of the C amount to total amount of Mo, Ti, Nb and V in percent by atom is 1.2 to 3; and
- a condition where the steel plate further contains at least two elements selected from Ti of about 0.005 to about 0.04%, Nb of about 0.005 to about 0.07% and V of about 0.005 to about 0.1%, wherein the remainder is substantially Fe, and C/(Ti+Nb+V) which is a ratio of the C amount to total amount of Ti, Nb and V in percent by atom is 1.2 to 3.
- 36. (Withdrawn) The method of claim: 35, wherein a metal structure of the hot-rolled steel plate is a substantially three-phase structure of ferrite, bainite and island martensite, and an area fraction of the island martensite is about 3 to about 20%.
- 37. (Withdrawn) A method for manufacturing a welded steel pipe, comprising:
  hot-rolling a steel slab, in which C of about 0.03 to about 0.1%, Si of about 0.01 to about
  0.5%, Mn of about 1.2 to about 2.5%, Al of about 0.08% or less, Mo of about 0.05 to about 0.4%
  and Ti of about 0.005 to about 0.04% are contained, and the remainder is substantially Fe, and
  C/(Mo+Ti) which is a ratio of C amount to total amount of Mo and Ti in percent by atom is 1.2
  to 3, at a condition of heating temperature of about 1000 to about 1300°C and rolling finish
  temperature of about Ar3 or more;

 performing accelerated cooling of the hot-rolled steel plate to about 450 to about 650°C at a cooling rate of about 5 °C/sec or more;

reheating the steel plate to about 550 to about 750°C at a heating rate of 0.5 °C/sec or more promptly after the cooling;

and forming a steel plate, in which a metal structure is a substantially three-phase structure of ferrite, bainite, and island martensite, and an area fraction of the island martensite is about 3 to about 20%, into a tubular shape in cold working, and then welding abutting surfaces to form a steel pipe.

## 38. (Withdrawn) A method for manufacturing a welded steel pipe comprising:

hot-rolling a steel slab, in which C of about 0.03 to about 0.1%, Si of about 0.01 to about 0.5%, Mn of about 1.2 to about 2.5%, and Al of about 0.08% or less are contained, and at least two selected from Ti of about 0.005 to about 0.04%, Nb of about 0.005 to about 0.07%, and V of about 0.005 to about 0.1% are contained, and the remainder is substantially Fe, and C/(Ti+Nb+V) which is a ratio of C amount to total amount of Ti, Nb and V in percent by atom is 1.2 to 3, at a condition of heating temperature of about 1000 to about 1300°C and rolling finish temperature of about Ar3 or more;

performing accelerated cooling of the hot-rolled steel plate to about 450 to about 650°C at a cooling rate of about 5 °C/sec or more;

reheating the steel plate to about 550 to about 750°C at a heating rate of about 0.5 °C/sec or more promptly after the cooling;

and forming a steel plate, in which a metal structure is a substantially three-phase structure of ferrite, bainite, and island martensite, and an area fraction of the island martensite is about 3 to about 20%, into a tubular shape in cold working, and then welding abutting surfaces to form a steel pipe.

- 39. (Withdrawn) The method according to any one of claims 35 to 38, wherein when the steel plate or steel pipe is reheated, it is reheated to temperature at least about 50°C higher than previously cooled temperature after the cooling.
- 40. (Withdrawn) The method according to any one of claims 35 to 38, comprising:

  performing the accelerated cooling to the hot-rolled steel plate to about 450 to about

  650°C at the cooling rate of about 5 °C/sec or more to form a two-phase structure of non
  transformed austenite and bainite; and

reheating the steel plate to about 550 to about 750°C at the heating rate of about 0.5 °C/sec or more promptly after the cooling to change the structure into a three-phase structure of a ferrite phase in which precipitates are dispersedly precipitated, a bainite phase and island martensite.

- 41. (Withdrawn) The method according to any one of claims 35 to 38, wherein the treatment of reheating the steel plate to about 550 to about 750°C at the heating rate of about 0.5 °C/sec or more promptly after cooling is performed with an induction heating device arranged on the same line as rolling equipment and cooling equipment.
- 42. (Withdrawn) The method according to any one of claims 35 to 38, wherein any one of the following complex carbides is precipitated in the ferrite phase:
  - (a) a complex carbide containing Ti and Mo, having a grain diameter of less than about 10nm, or
  - (b) a complex carbide containing Ti, Mo, Nb, and/or V, having a grain diameter of less than about 10nm, or
  - (c) a complex carbide containing at least two elements selected from Ti, Nb and V, having a grain diameter of less than about 10nm.

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- 43. (Withdrawn) The method according to any one of claims 35 to 38, wherein the plate or the pipe further contains N of about 0.007% or less by mass.
- 44. (Withdrawn) The method according to claim 37, wherein the plate or the pipe further contains Nb of about 0.005 to about 0.07% and/or V of about 0.005 to about 0.1%, and C/(Mo+Ti+Nb+V) that is a ratio of C amount to total amount of Mo, Ti, Nb and V in percent by atom is 1.2 to 3.
- 45. (Withdrawn) The method according to any one of claims 35 to 38, wherein the plate or the pipe further contains Ti of about 0.005 to less than about 0.02%.
- 46. (Withdrawn) The method according to any one of claims 35 to 38, wherein the plate or the pipe further contains at least one element selected from Cu of about 0.5% or less, Ni of about 0.5% or less, Cr of about 0.5% or less, B of about 0.005% or less, and Ca of about 0.0005 to about 0.003% by mass.
- 47. (Withdrawn) The method according to any one of claims 35 to 38, wherein the plate or the pipe further contains Ti/N of about 2 to about 8 in percent by mass.
- 48. (Withdrawn) The method according to any one of claims 35 and 36, further comprising forming obtained steel plates into a tubular shape in cold working, and welding abutting surfaces to form a steel pipe.